#### Kinetic Parameters Estimation in a MTR Research and Production Reactor in Subcritical States



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## **Objectives**

#### Kinetic parameters estimation

- Inverse kinetics as a reactimeter in subcritical states (monitoring a refueling operation).
- Determination of the strength of the neutron source (point kinetic model).
- Characterization of the neutron source. Photoneutron effectiveness estimation  $(\gamma^{ph})$ .
- Neutron noise technique in presence of  ${}^{135}Xe$  and high gamma exposure rate  $(10^6 R/h)$ .
- Reactivity and power estimations  $(30 \, mW$  to  $200 \, mW)$ .



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#### Neutron source

#### Photoneutrons

- Produced in the reaction  $D(\gamma, n)H$  for  $E_{\gamma} > 2,23 \, MeV$
- Treated as nine extra groups of delayed neutrons in the point kinetic equations.
- Assumed to come from precursors originated during the normal operation of the reactor at full power.
- Measurements were made 36 h after the reactor shutdown. The photoneutron source was assumed to be constant during each measurement (~ h).



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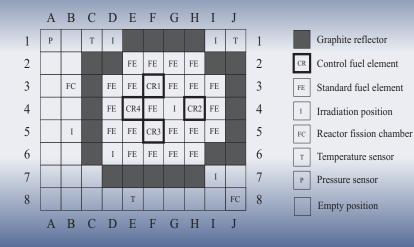
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Experimental procedure



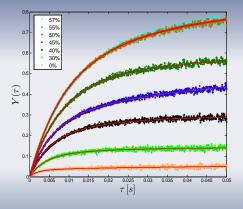
## **RA-3** core configuration



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#### Neutron noise technique



Reactivities: -6 < \$ < -0.5Count rate:  $1 \, 10^5 cps < R < 7 \, 10^5 cps$ 

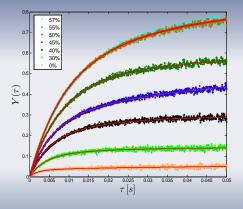
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|---|
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D: Diven factor  $\Lambda$ : Neutron generation time  $\epsilon$ : Absolute efficiency ( $\sim$  Power)  $\alpha$ : Prompt neutron decay constant

Power and reactivity are estimated in each stationary subcritical state.



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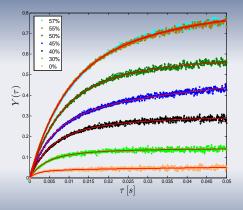
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## Estimation of $\alpha_c$

$$\alpha = \alpha_{c} + \frac{\tilde{S}}{R}$$

By measuring  $\alpha$  and R at different subcritical states a linear fit can be performed to obtain  $\alpha_c$ .

$$\alpha_c = (106 \pm 1)s^{-1}$$



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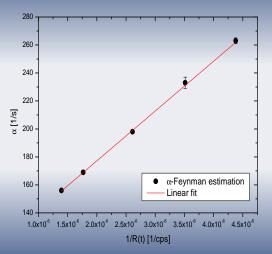




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At each subcritical state:  $\alpha = \alpha_c + \frac{\tilde{S}}{R}$ 

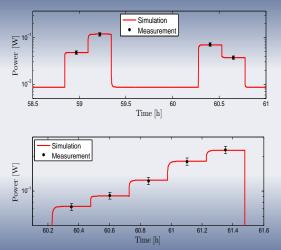
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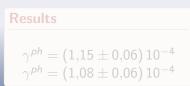
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## Estimation of $\gamma^{ph}$

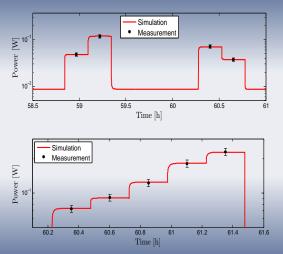


Parametric variation of  $\gamma^{ph}$  in the point kinetics equations until the best fit of the simulation to the measured power is found.

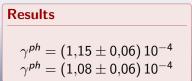




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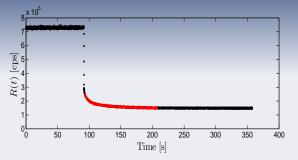
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#### Least square inverse kinetics method



Rod-drop between two subcritical states.

Transient evolution is fitted with a linearized model (LSIKM).

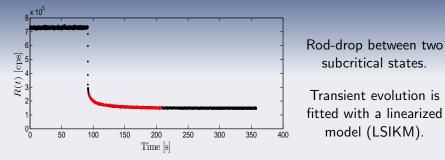
$$R(t) = \frac{\Lambda^*}{\$_f - 1} \tilde{Q}(t) - \frac{\Lambda^* S}{\$_f - 1}$$

Measuring R(t) and  $\bar{Q}(t)$  one can obtain the final state reactivity  $(\$_f)$  and the source strength  $(\tilde{S})$ .

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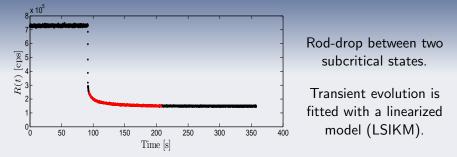
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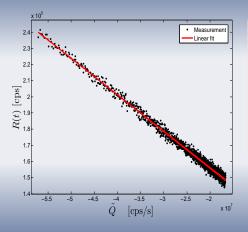
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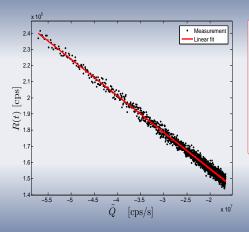


# Estimated values • Detector at G8 $\tilde{S} = (6,90 \pm 0,04) \, 10^6 \, cps/s$ • Detector at B1 $\tilde{S} = (2,6 \pm 0,1) \, 10^6 \, cps/s$

depends on the detector efficiency However,it is the magnitude that appears in the inverse kinetics.



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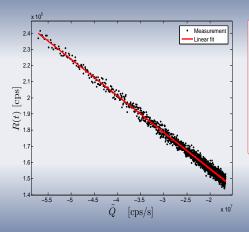


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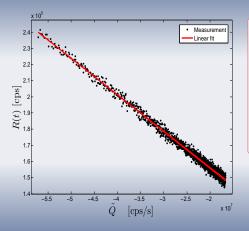


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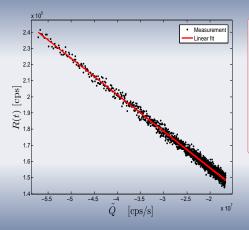


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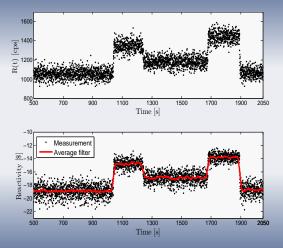
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## Subcritical reactimeter

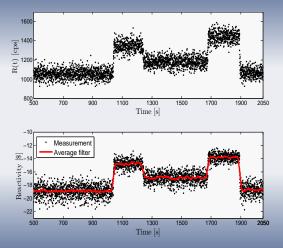


With the estimation of  $\tilde{S}$ , the reactivity can be obtained measuring the count rate during a refueling operation.

#### **Refueling operation**

- Extraction CR from F5
- Extraction FE from F5
- Entering fresh FE at F5

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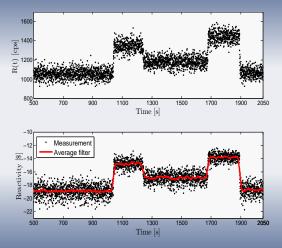


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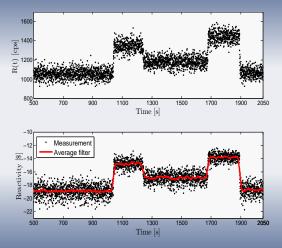


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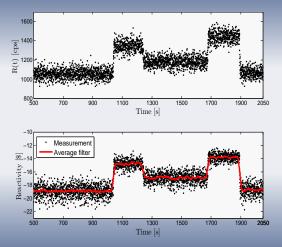


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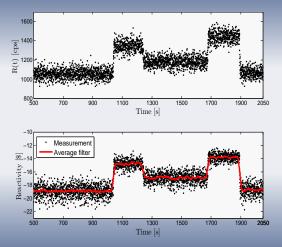


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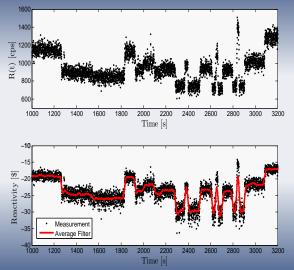
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## Subcritical reactimeter



#### Core 212 to 213

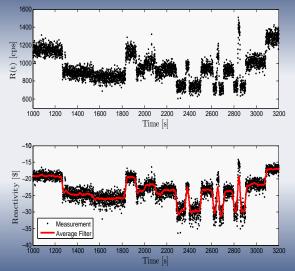
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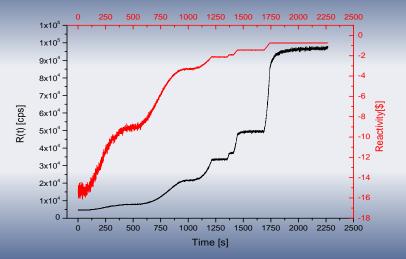
#### Core 212 to 213

Extraction of burned FE, rotation and entering fresh FE

At these highly subcritical levels, spatial effects become important in reactivity estimations.



### Approach to critical



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### Numerical model

**Diffusive code PUMA** 

Using a homogeneous neutron source in all the fuel channels (First step)  $% \left( \left( F_{1},F_{2},F_{1},F_{2},F_{1},F_{2},F_{1},F_{2},F$ 

- As the magnitude of the neutron source was not known in advance, all the comparisons were made relative to the first state.
- A refueling operation was calculated



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# Results from core 212 to 213

| Core            | Experimental |                 | PUMA  |           |                 |
|-----------------|--------------|-----------------|-------|-----------|-----------------|
| configuration i | $R_i/R_0$    | $\rho_0/\rho_i$ | φi/φ0 | $P_i/P_0$ | $\rho_0/\rho_i$ |
| Core 212 0      | 1            | 1               | 1     | 1         | 1               |
| 1               | 0.78 (3)     | 0.8 (1)         | 0.784 | 0.910     | 0.928           |
| 2               | 0.74 (3)     | 0.7 (1)         | 0.740 | 0.788     | 0.809           |
| 3               | 0.98 (4)     | 1.00 (5)        | 0.962 | 0.878     | 0.885           |
| 4               | 0.82 (3)     | 0.8 (1)         | 0.806 | 0.915     | 0.939           |
| 5               | 0.81 (3)     | 0.8 (1)         | 0.787 | 0.884     | 0.901           |
| 6               | 0.88 (4)     | 0.9 (1)         | 0.821 | 0.783     | 0.787           |
| Core 213 7      | 1.11 (4)     | 1.12 (5)        | 1.113 | 1.090     | 1.081           |



### Numerical model

#### **Future improvements**

- Calculate the photoneutron source.
- ORIGEN with the information of each FE.
- MCNPX to obtain the photoneutron source.
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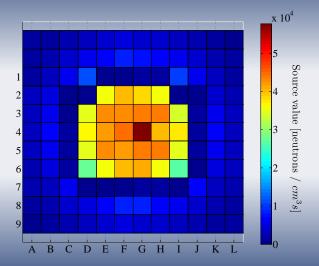
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# Photoneutron source (MCNPX)





# Conclusions

- Measurements at subcritical states with high gamma background and  $^{135}Xe$ .
- With the neutron noise technique reactivities were estimated between −6 and −0,5 dollars. Power between 30 mW and 200 mW.
- First estimations of the pohotoneutron effectiveness  $\gamma^{ph} = (1.12 \pm 0.06) \, 10^{-4}$
- Estimation of the source strength value  $(\tilde{S})$  that appears in the point kinetics equation.
- Using the inverse kinetics as a subcritical reactimeter
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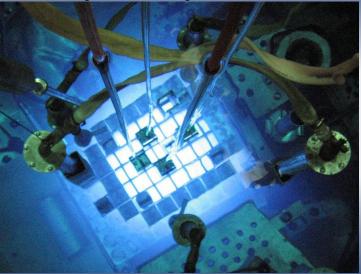
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# Thank you for your attention



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